

# An Evanescent Wave Fluorescence Fiber-Optic Flow Sensor for Resin Transfer Molding

by Bruce K. Fink, Roopesh Mathur, and Suresh G. Advani

ARL-TR-2240 June 2000

Approved for public release; distribution is unlimited.

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

Citation of manufacturer's or trade names does not constitute an official endorsement or approval of the use thereof.

Destroy this report when it is no longer needed. Do not return it to the originator.

#### **Abstract**

An evanescent wave fluorescence-based fiber-optic flow sensor is being investigated. This sensor is based on the interaction of a laser beam in a bare optical fiber with fluorescent probe molecules present in the resin flowing in the direction of the fiber. The electric field of the monochromatic light waves traveling in the fiber by total internal reflection penetrates outside the fiber and is called the evanescent wave field. A fluorescent probe molecule within the depth of penetration gets excited by this field and emits a characteristic fluorescent radiation that is coupled back into the fiber by the principle of reciprocity of optics. If the light at the end of the fiber is filtered for the fluorescent radiation and the intensity is recorded, it gives an estimate of the number of fluorescent probe molecules in contact with the fiber and, hence, the extent to which the fiber is covered with the resin. Preliminary experiments have shown that there is a linear correlation between the peak intensity and the length of fiber in contact with the fluid. A laboratory setup has been assembled at the University of Delaware (UD), using a photomultiplier-tube-based detector, and various experiments have been conducted to assess the effect of covered fiber length on the intensity of fluorescence using the evanescent mode of sensing and on the uses of distal mode sensing of fluorescence for detection of flow.

### Acknowledgments

This research was supported in part by the U.S. Army Research Laboratory (ARL)-sponsored Composite Materials Research Program at the University of Delaware. The authors would like to acknowledge Dr. George H. Watson and Mr. Ranjit D. Pradhan of the Department of Physics, University of Delaware, for aiding in the construction of the experimental facility at the University of Delaware. Mr. Sean Gallagher carried out the experiments at Delaware. The preliminary experiments were performed at the Polymers Division (National Institute of Standards and Technology [NIST]) with the help of Dr. Richard Parnas and Dr. Joy Dunkers (NIST), Dr. Dara Woerdman (Johns Hopkins University), and Mr. Robert Lowry (NIST).

INTENTIONALLY LEFT BLANK.

### **Table of Contents**

		Page
	Acknowledgments	iii
	List of Figures	vii
1.	Introduction	1
2.	Theory	3
3.	Experimental Setup	5
4.	Experiments	6
5.	Results and Conclusions	8
6.	References	13
	Distribution List	17
	Report Documentation Page	37

INTENTIONALLY LEFT BLANK.

## **List of Figures**

Fig	<u>ure</u>	Page
1.	Schematic of Experimental Setup	5
2.	Plot of Intensities of Fluorescence Detected Using a CCD Detector Array With Wavelengths of Light for Different Lengths of Fiber Covered	8
3.	Plot of Peak Fluorescent Intensity at 570 nm Detected Using a CCD Detector at NIST for Different Lengths of Fiber Covered by a Solution of Rhodamine B in Ethanol	9
4.	Plot of Change in Intensity Detected as Fluorescent Dye Flows Past the Tip of the Optical Fiber	9
5.	Plot of Peak Fluorescent Intensity at 570 nm Detected Using a Photon Counter for Different Lengths of Optical Fiber Covered by a Solution of Rhodamine B in Ethanol (Experiments 1 and 2)	10
6.	Plot of Peak Fluorescent Intensity at 570 nm Detected Using a Photon Counter for Different Lengths of Optical Fiber Covered by a Solution of Rhodamine B in Ethanol (Experiment 3)	11
7.	Plot of Peak Fluorescent Intensity at 570 nm Detected Using a Photon Counter for Different Lengths of Optical Fiber Covered by a Solution of Rhodamine B in Ethanol (Experiments 4 and 5)	11

INTENTIONALLY LEFT BLANK.

#### 1. Introduction

Resin transfer molding (RTM) is a versatile and economic process for the manufacture of polymer composites. RTM is finding increasing acceptance in the fabrication of large and complex parts. Due to their high strength-to-weight ratio, composites have been developed for a number of industrial and aerospace applications as an attractive alternative to conventional metallic parts. However there is a significant need to improve the quality and process control of the RTM processes. The variability of processing conditions and the state of the raw materials cause large part-to-part variations. Thus, there is a need to improve the efficiency and reliability of composite processing.

Modeling and simulation have been used with some success to gain insight into the complex phenomena during flow and cure of resin. The liquid-injection molding simulation software (LIMS) developed at the University of Delaware has been used to predict the occurrence of dry spots occurring when resin flows in molds with complex geometries [1–6].

Another way to improve the efficiency and reliability of a manufacturing process is through the implementation of an on-line sensing-and-control system. This would allow the production of parts with consistently high quality. Hence, there has been considerable work done in the area of on-line sensing techniques. A number of in-situ sensors have been developed for the composite manufacturing processes such as electromagnetic, ultrasonic, spectrometric, and fluorescence sensors [7, 8].

The changes in electromagnetic responses between sensing elements, separated spatially in the mold, as the resin flows and cures have been widely used in many sensors [9–13]. As the resin flows between the elements, it completes an electrical circuit, providing the signal that the resin has reached that point. As the resin cures, there is a change in the permittivity due to decreasing ionic mobility of the adventitious ions, and this can be correlated to the state of the cure.

Ultrasonic wave-based techniques have been used as tools to detect the cure of epoxies [14, 15]. Ultrasonic waves are passed through the composite part, and the phase velocity and attenuation are measured. As the resin cures the changes in elastic, bulk and relaxation moduli of the resin change, thus changing the speed of propagation, as well as damping of the ultrasonic waves. Some common problems associated with this technique are the low signal-to-noise ratio, dispersion and scattering of the waves, and limitations on the temperature and pressure of operation.

Spectroscopic techniques have been used to detect the cure of composite parts [15-24]. Some of these techniques are ultraviolet (UV)-visible (Vis) and infrared (IR) spectroscopy, fluorescence spectroscopy, and Raman spectroscopy. All of these techniques involve the scattering interaction of a monochromatic beam of light, usually from a laser or a filtered incandescent lamp with the material. The intensity and wavelength of the scattered light yields information about the material under study. In IR spectroscopy, each bond in the resin system has its characteristic peak in the absorption spectrum. Thus, as some bonds form and others get broken during the curing process, the intensities at the corresponding peaks change. In UV-Vis and fluorescence spectroscopy, the light photon excites the molecule to a characteristic energy level. The molecule then de-excites to a lower energy level, emitting a characteristic photon. In a resin system, as the monomer molecules cross-link, the vibrational and translational degrees of freedom get restricted. Thus, the amount of energy available for excitation is higher. This leads to increasing intensity of the emission spectrum, as well as a blue shift as the wavelength of the photons decreases. In Raman spectroscopy, the excitation photon does not have enough energy to excite the molecule to the next energy level. Hence, the energy absorption lifts the photon to a virtual vibrational energy level below the first electronic state. Within a short time, it returns to a stable energetic level in the ground electronic state. If this state is not the same as the original state, then the emission photon has a different wavelength than the excitation light. This shift is called the Raman shift and is characteristic of the molecule. The intensity of the Raman spectrum is directly proportional to the concentration of the chemical species and related to the temperature of the specimen [20]. Hence resin cure can be detected by measuring the decreasing concentration of the epoxide. All these spectroscopic techniques are noncontact; work by direct molecular-level interaction; and, hence, provide a primary measure of cure. However, the effects of the temperature on the spectra obtained have to be compensated in order to get accurate data.

Fiber optics have been used for remote in-situ spectroscopy [20–36]. The excitation beam is conveyed by the fiber to the region of interest; hence, the fiber optic sensor can be used as both a surface sensor and as an embedded sensor in composites processing. The size of the fiber-optic probe is comparable to the size of the reinforcement fibers in composites. Hence, the interference effects are minimal. The two modes of sensing using fiber optics are (1) the distal mode and (2) the evanescent mode of sensing. In the distal mode, the end of the sensor is in contact in the specimen and is used to sense in a small volume surrounding the tip. In evanescent wave sensing, the interaction of the evanescent electric field of the monochromatic light propagating in the fiber with the surroundings is used for sensing. Thus, the full length of the fiber acts as a probe. It is expected that, as the fiber gets covered, the intensity of the detected signal will increase. In earlier work [35-37], a corresponding blue shift in peak intensity was seen as resin cure progressed. This enables the development of a inexpensive fiber-optic flow and cure sensor, which can be used to investigate the flow into fiber bundles and flow in molds with complex geometry. Thus, fiber-optic evanescent wave sensors have been investigated in an ongoing collaboration between the U.S. Army Research Laboratory (ARL) and the National Institute of Standards and Technology (NIST).

A fiber-optic evanescent wave-based flow sensor is presented here. An argon ion laser was made to interact with a fluorescent dye solution flowing along the length of the fiber optic, and the resultant signal from the fluorescence interaction was monitored using an intelligent photo sensor. An experiment based on distal mode sensing was also conducted.

#### 2. Theory

Optical fibers transmit light by total internal reflection. Light focused on the end face of the fiber intersects the fiber-medium interface at an angle determined by Snell's law. If the refractive index of the medium is less than that of the fiber, then there exists a critical angle of

incidence beyond which the light gets reflected back into the fiber. Thus, light propagating in the fiber at an angle greater than this propagates through the fiber. The electric field amplitude of the guided wave decays exponentially in the medium.

The evanescent wave fluorescent wave sensor is based on the interaction of the fluorescent dye molecules with the evanescent electric field. It is necessary that the refractive index of the sensor be higher than that of the surrounding medium. At the interface between the wave guide and the medium, the light suffers total internal reflection. The evanescent filed arises from the interference between the electric fields of the incoming and the reflected rays. The evanescent wave extends beyond the reflecting interface into the surrounding medium and decays exponentially in amplitude. The distance to which the electric field decays to (1/e) its original value is called the depth of penetration. This depth of penetration is given by

$$d_{p} = \frac{\lambda}{2\pi(\sin^{2}\theta - (n_{2}/n_{1})^{2})^{1/2}},$$
(1)

where  $\lambda$  is the wavelength of the light,  $n_1$  is the refractive index of the fiber,  $n_2$  is the index of the medium, and  $\theta$  is the angle of incidence of the propagating light at the interface. Values for  $d_p$  are of the order of 100–10,000 nm.

We select the angles of incidence at the fiber front to be less than the critical angle so that there are no losses at the face. The amplitude decays exponentially with the distance. The probability of fluorescence is dependent on the product of quantum efficiency of fluorescence and the probability of absorption of the evanescent photon. It is estimated that approximately half the light is emanating from fluorescence at a distance z, where the evanescent wave amplitude is significant. The efficiency of collection and transmission of the fluorescence is dependent on whether the angle in the fiber is greater than the critical angle or not. Almost all the fluorescence in the fiber will be lost for angles less than the critical angle, as can be expected. By the principle of reciprocity of optics, one can expect that, if the emission of the excited molecule itself is evanescent, then the fluorescent photons that get into the fiber will get

internally reflected and will reach the detector, whereas the fluorescent light that gets refracted into the fiber by the principles of conventional ray optics will lose intensity rapidly with each successive reflection as part of the ray gets refracted into the medium and will therefore be very weak at the detector. Hence, the chief component of the detected fluorescence at the detector end will be the evanescent wave fluorescence. Since the intensity of the electric field of the monochromatic light is approximately the same at every point on the fiber where the laser beam reflects off the fiber-medium interface and nearly all the evanescent wave photons reach the detector, there is a linear correlation between the intensity detected and the length of the fiber in contact with the fluorescent solution. However, there will be a sudden increase in intensity as the conventional fluorescent rays that enter the fiber very near the detector end have not dissipated through losses.

### 3. Experimental Setup

An optical bench (Figure 1) was constructed for the flow monitoring experiments. The experimental setup consisted of an Ar+ laser, a system of mirrors, beam splitter, 20X microscope objective and a fiber coupler to couple the laser light into the NIST-supplied leaded glass fiber-optic cable.

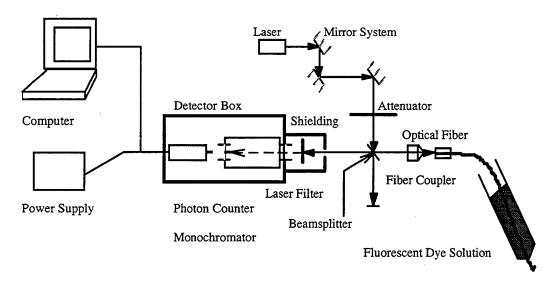


Figure 1. Schematic of Experimental Setup.

The detection system at the University of Delaware consisted of a laser filter, monochromator, and a intelligent photosensor module (Hammamatsu HC-135 sensor). The wavelength on the monochromator was set using a stepper motor interfaced to the shaft using a flexible coupling. The stepper motor and the intelligent photosensor were interfaced to a PC (P5-166) for control and data acquisition purposes.

The intelligent photosensor combines the sensitivity of a photomultiplier tube with the intelligence of a microcontroller to provide a flexible and sensitive detector that can be interfaced to the computer very easily using a standard RS-232 cable to the serial port. The detector module acquires the signal by counting the number of photons as they enter the input window. This is the most sensitive technique available for light measurement. The photon-counting sensor has a large active area of diameter 21 mm for light gathering. The photomultiplier tube does the photon counting using a series of cascade circuits that generate thousands of electrons for every photon impinging on the light gathering area. The photomultiplier tube is powered by an onboard high-voltage Cockroft-Walton power supply. This is used to limit current consumption and prevent unwanted temperature rise of the assembly. The photosensor is powered by a direct-current (DC) power supply rated at a voltage of 5 V.

The light signal from the photomultiplier tube takes the form of very high current pulses. These pulses are amplified and converted to digital pulses with a high-speed amplifier and discriminator. They are then prescaled by a value of four before counting, which increases the dynamic range without using excessive power. These pulses are counted using by the microcontroller. The HC-135 integrates all the necessary components required for photon counting in a compact cylindrical body of diameter 1.35 in and length of 5 in.

### 4. Experiments

A fiber-optic flow sensor can be implemented in two modes of sensing. In the first mode, called distal mode sensing, the fiber-optic sensor is a point sensor. The optical fiber acts as a conduit for the laser beam to reach a point in space. When the flow containing fluorescent dye

reaches the tip of the fiber, which is illuminated by the laser beam, the dye molecules get stimulated and emit fluorescent photons. This radiation gets conducted back along the fiber and goes to the detector, which is set up to receive only those photons of the wavelength corresponding to the peak of the spectrum of fluorescence of the dye. The change in signal immediately indicates that the flow has reached that point. In the second mode of sensing, the evanescent mode, the entire length of the optical fiber acts as a sensor. The dye is made to flow along the length of the fiber and the change in signal recorded as the optical fiber gets progressively covered.

A number of experiments were carried out to detect the flow of a solution of Rhodamine B dissolved in ethanol to a concentration of 10<sup>-6</sup> M. The optical fiber used, that was supplied by the Polymers Division, NIST, had a high refractive index of 1.6. The intensity of background light was measured using the photon counter with the lights off. The "dark count" of the detector (i.e., the photon counts obtained when the detector is closed off to all sources of external light using a cap) was found to be of the order of 150 counts/second. The background and fluorescent photon counts were of the order of 100,000 counts/second. Hence, the dark count was neglected in subsequent calculations. The background count was subtracted from the subsequent readings in order to obtain an accurate estimate of the fluorescent light reaching the detector. The monochromator was set to 570 nm, which is the maximum of the spectrum obtained for the fluorescence of Rhodamine B dye dissolved in ethanol. The laser was turned on, and the background count was recorded to give a baseline for subsequent readings. In the first series of experiments for distal mode sensing, the optical fiber was suspended inside the tube and the fluorescent dye solution was injected from the bottom until it reached the fiber tip. At that point, the change in the counts was recorded. This change in counts is plotted.

A number of experiments were performed to evaluate the evanescent mode of sensing. The optical fiber was run through the tube and clamped at the end. The tip of the fiber extending below the tube was blackened in order to prevent background light from getting conducted to the detector through the fiber. A centimeter scale was attached to the tube. The dye solution was injected along the length of the fiber. At every centimeter graduation, the photon count was

recorded until the tube filled up completely. The background count was subtracted and the fluorescent count plotted against length of fiber covered.

A few preliminary experiments were conducted at NIST in order to explore use of the fiber-optic flow sensor. A charged coupling device (CCD) camera was used for detection of fluorescent intensities at different wavelengths. The fluorescent spectra were recorded as the fiber length was covered progressively. The spectra are shown in Figure 2. As can be observed, the peak intensity shows an increase. When plotted against the length of fiber covered the peak intensity shows a linear variation with a jump at the end (Figure 3).

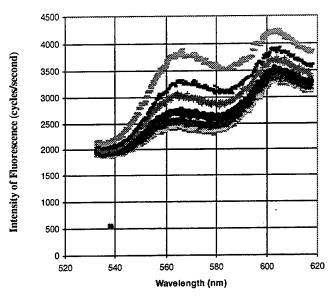


Figure 2. Plot of Intensities of Fluorescence Detected Using a CCD Detector Array With Wavelengths of Light for Different Lengths of Fiber Covered. (Experiment Conducted at NIST.)

#### 5. Results and Conclusions

The results from the various experiments were plotted for both the distal mode (Figure 4) and the evanescent mode experiments. In the experiments with distal mode sensing, a significant increase in signal was observed as the flow reached the tip of the optical fiber. The data from the

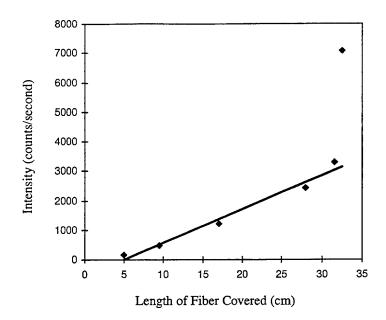


Figure 3. Plot of Peak Fluorescent Intensity at 570 nm Detected Using a CCD Detector at NIST for Different Lengths of Fiber Covered by a Solution of Rhodamine B in Ethanol.

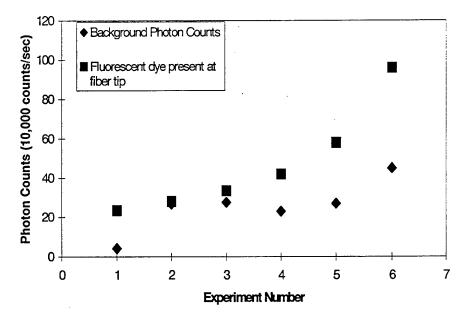


Figure 4. Plot of Change in Intensity Detected as Fluorescent Dye Flows Past the Tip of the Optical Fiber.

experiments demonstrates that a fiber-optic point flow sensor is feasible. During the filling process in mold filling and cure, feedback from a point sensor can provide vital information for on-line control and for triggering decision points.

In the evanescent mode of sensing using optical fibers (Figures 5–7), it was observed that, as the fiber was covered by the dye, there was an increase in signal that was fairly linear in nature. This linearity is predicted by the theory of the evanescent wave fiber-optic sensors. The abrupt increase in signal at the end can be caused by the bulk fluorescence of the dye solution due to leakage of light from the optical fiber. This bulk fluorescence usually dissipates through repeated refractions and reflections at the uncovered part of the surface of the optical fiber and does not reach the detector. As the flow nears the detector, the numerous photons of bulk fluorescence have a smaller distance to travel to register at the detector. Hence, the photon count registers an increase. The intensity of the bulk fluorescence is proportional to the number of dye molecules in the volume surrounding it and, hence, to the length of fiber covered. Thus, the linearity of the signal is still preserved.

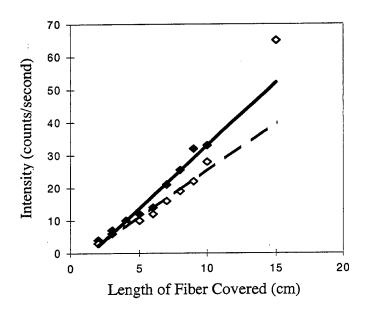


Figure 5. Plot of Peak Fluorescent Intensity at 570 nm Detected Using a Photon Counter for Different Lengths of Optical Fiber Covered by a Solution of Rhodamine B in Ethanol (Experiments 1 and 2).

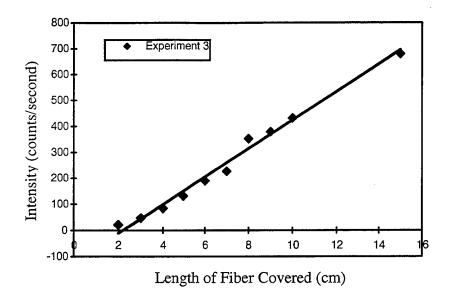


Figure 6. Plot of Peak Fluorescent Intensity at 570 nm Detected Using a Photon Counter for Different Lengths of Optical Fiber Covered by a Solution of Rhodamine B in Ethanol (Experiment 3).

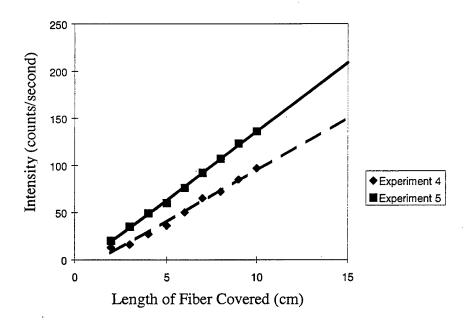


Figure 7. Plot of Peak Fluorescent Intensity at 570 nm Detected Using a Photon Counter for Different Lengths of Optical Fiber Covered by a Solution of Rhodamine B in Ethanol (Experiments 4 and 5).

The experiments show that an evanescent wave fluorescence fiber-optic sensor is a distinct possibility. The linearity of the signal can enable the detection of flow in a mold filling process in any given direction in an "analog" fashion. The reaction time is very small, and the optical fiber may be woven into the preform. This would enable the sensing of flow in complicated molds and in molds for manufacturing thick parts, where the sensors currently in use, which are surface mounted, are inadequate. Further, the optical fiber is of the same size as most preform tows and it would not affect the resin flow. In fact, it may be used for monitoring strains due to loading in the composite part, after manufacture.

#### 6. References

- 1. Bruschke, M., and S. G. Advani. "A Finite Element/Control Volume Approachto Mold Filling in Anisotropic Porous Media." *Polymer Composites*, vol. 11, pp. 398–405, 1990.
- 2. Bruschke, M. V., and S. G. Advani. "RTM: Filling Simulation of Complex Three-Dimensional Shell-Like Structures." *SAMPE Quarterly*, vol. 23, no. 1, pp. 2–11, 1991.
- 3. Bruschke, M. V., and S. G. Advani. "A Numerical Approach to Model Non-Isothermal, Viscous Flow With Free Surfaces Through Fibrous Media." *International Journal of Numerical Methods in Fluids*, vol. 19, pp. 575–603, 1994.
- 4. Liu, D., S. Bickerton, and S. G. Advani. "Modeling and Simulation of RTM: Gate Control, Venting and Dry Spot Prediction." *Composites Part A*, vol. 27A, pp. 135–141, 1996.
- 5. Maier, R. S., T. F. Rohaly, S. G. Advani, and K. D. Fickie. "A Fast Numerical Method for Isothermal Resin Transfer Mold Filling." *International Journal of Numerical Methods in Engineering*, vol. 39, pp. 1405–1422, 1996.
- 6. Fong, L. L., B. Liu, R. R. Varma, and S. G. Advani. "Liquid Injection Molding Simulation User Manual, Version 3.4." Technical Report, Center for Composite Materials, University of Delaware, 1996.
- 7. Hunston, D. L., W. McDonough, B. Fanconi, F. Wang, F. Phelan, and M. Chiang. "Assessment of the State of the Art for Process Monitoring Sensors for Polymer Composites." NISTIR 4514, National Institute of Standards and Technology, pp. 73–108, 1991.
- 8. Jang, B. Z., and W. K. Shih. "Techniques for Cure Monitoring of Thermoset Resins and Composites A Review." 1990 Materials and Manufacturing Processes, vol. 5, no. 2, pp. 201–331.
- 9. Ciriscioli, P. R., and G. S. Springer. "Dielectric Cure Monitoring A Critical Review." 34th International SAMPE Symposium Proceedings, p. 312, 1989.
- 10. Fink, B. K., S. M. Walsh, D. C. DeSchepper, J. W. Gillespie, Jr., R. L. McCullough, R. C. Don, and B. J. Waibel. "Advances in Resin Transfer Molding Flow Monitoring Using SMARTWEAVE Sensors." *Proceedings of the ASME International Mechanical Engineering Conference*, pp. 999-1015, 1995.

- 11. Mijovic, J., J. M. Kenny, B. K. Fink, S. M. Walsh, D. C. DeSchepper, J. W. Gillespie, Jr., R. L. McCullough, R. C. Don, and B. J. Waibel. "The Principles of Dielectric Measurements for In Situ Monitoring of Composite Processing." *Composites Sciences and Technology*, vol. 49, p. 277, 1993.
- 12. England, K. M., J. W. Gillespie, Jr., and B. K. Fink. "In-Situ Sensing of Viscosity by Direct Current Measurements." *Proceedings of the International Mechanical Engineering Congress and Expo*, American Society of Mechanical Engineers, 1996.
- 13. Schwab, S., R. L. Levy, and G. G. Glover. "Sensor System for Monitoring Impregnation and Cure During Resin Transfer Molding." *Polymer Composites*, vol. 17, no. 2, 1996.
- 14. Lindrose, A. M. "Ultrasonic Wave and Moduli Changes in a Curing Epoxy Resin." Experimental Mechanics, p. 227, July 1978.
- 15. Tuegel, E. J., and T. H. Hahn. "Ultrasonic Cure Characterisation of Epoxy Resins: Constitutive Modeling." Advances in Modeling of Composites Processes, 1985.
- 16. Pyun, K., C. Sung. Network Structure in Diamine-Cured Tetrafunctional Epoxy by UV-Visible and Fluorescence Spectroscopy." *Journal of the American Institute of Chemical Engineers*, 1991.
- 17. Yu, W., and C. Sung. "Excitation Spectroscopy of a Reactive Label for Characterization of the Cure Process in an Epoxy Network." *Macromolecules*, vol. 23, pp. 386–390, 1990.
- 18. Sung, C., E. Pyun, and H. L. Sun. "Characterization of Epoxy Cure by UV-Visible and Fluorescence Spectroscopy: Azochromophoric Labelling Approach." *Macromolecules*, vol. 19, pp. 2922–2932, 1986.
- 19. Kim, Y. S., and C. Sung. "UV and Flourescence Characterization of Styrene and Methyl Methacrylate Polymerization." *Journal of Applied Polymer Science*, vol. 57, pp 363–370, 1995.
- 20. Stroeks, A., M. Shmorhun, A. M. Jamieson, and R. Simha. "Cure Monitoring of Epoxy Resins by Excimer Flourescence." *Polymer*, vol. 29, pp. 467–470, March 1988.
- 21. Stellman, C. M., J. Aust, and M. Myrick. "In-Situ Spectroscopic Study of Microwave Polymerisation." *Applied Spectroscopy*, vol. 49, no. 3, pp. 392–394, 1995.
- 22. Paik, H., and N. Sung. "Fiberoptic Intrinsic Flourescence for In-Situ Cure Monitoring of Amine Cured Epoxy and Composites." *Polymer Engineering and Science*, vol. 34, no. 12, pp. 1025–1031, 1994.

- 23. Radhakrishnan, S., and R. A. Pethrick. "Continuous UV Cure Monitoring and Dielectric Properties of Photocross-Linked Epoxy-Acrylate Resins." *Polymer Engineering and Science*, vol. 51, pp. 863–871, 1994.
- 24. Lyon, R. E., K. E. Chike, and S. M. Angel. "In-Situ Cure Monitoring of Epoxy Resins Using Fiber Optic Raman Spectroscopy." *Journal of Applied Polymer Science*, vol. 53, pp. 1805–1812, 1994.
- 25. Mayinger, F. "Optical Measurements, Techniques and Applications." Chap. 9, Springer-Verlag, 1994.
- 26. Wang, F. W., and B. Fanconi. "In-Situ Characterization of the Interface of Glass Reinforced Composites." National Bureau of Standards Internal Report No. 87–3581, 1987.
- 27. Wang, F. W., R. E. Lowry, and B. M. Fanconi. "Novel Fluorescence Method for Cure Monitoring of Epoxy Resins." *Polymer*, vol. 27, pp. 1529–1532, 1986.
- 28. Blair, D. S., L. W. Burgess, and A. M. Brodsky. "Study of Analyte Diffusion Into a Silicone-Clad Fiber-Optic Chemical Sensor by Evanescent Wave Spectroscopy." *Applied Spectroscopy*, vol. 49, no. 11, 1995.
- 29. Fuh, M. R. S., L. W. Burgess, and G. D. Christian. "Single Fiber-Optic Fluorescence Enzyme-Based Sensor." *Analytical Chemistry*, vol. 60, pp. 433–435, 1988.
- 30. Degrandpre, M. D., and L. W. Burgess. "A Fiber Optic FT-NIR Evanescent Field Absorbance Sensor." *Applied Spectroscopy*, vol. 44, no. 2, pp. 273–279, 1990.
- 31. Conzen, J. P., J. Burck, H. J. Ache. "Characterization of a Fiber-Optic Evanescent Wave Absorbance Sensor for Nonpolar Organic Compounds." *Applied Spectroscopy*, vol. 47, no. 3, pp. 753–763, 1993.
- 32. Young, P. R., M. A. Druy, W. A. Stevenson, and D. A. Compton. "In-Situ Composite Cure Monitoring Using Infrared Transmitting Optical Fibers." *SAMPE Journal*, vol. 25, no. 2, pp. 11–16, 1989.
- 33. Ahn, S. H., W. L. Lee, and G. S. Springer. "Measurement of the Three-Dimensional Permeability of Fiber Preforms Using Embedded Fiber Optic Sensors." *Journal of Composite Materials*, vol. 29, no. 6, 1995.
- 34. Woerdman, D. L., and R. S. Parnas. "Cure Monitoring in RTM Using Fluorescence." Plastics Engineering, October 1995.

- 35. Woerdeman, D. L., K. L. Flynn, and R. S. Parnas. "Evanescent Wave Optical Fiber Sensors for Monitoring and Control of the Liquid Molding Process." *Proceedings of the 9th International Conference on Automated Composites*, Nottingham, England, September 1995.
- 36. Woerdeman, D. L., and R. S. Parnas. "Cure Monitoring With Evanescent Wave Fluorescence Sensor." Annual Technical Conference of the Society of Plastics Engineers 1995, pp. 2805–2811, 1995.

NO. OF		NO. OF	
COPIES	<u>ORGANIZATION</u>	COPIES	ORGANIZATION Property of the control
2	DEFENSE TECHNICAL	1	DIRECTOR
	INFORMATION CENTER		US ARMY RESEARCH LAB
	DTIC DDA		AMSRL D
	8725 JOHN J KINGMAN RD		D R SMITH
			2800 POWDER MILL RD
	STE 0944		ADELPHI MD 20783-1197
	FT BELVOIR VA 22060-6218		ADELPHI MD 20763-1197
1	TIODA	1	DIRECTOR
1	HQDA	•	US ARMY RESEARCH LAB
	DAMO FDT		AMSRL DD
	400 ARMY PENTAGON		
	WASHINGTON DC 20310-0460		2800 POWDER MILL RD
			ADELPHI MD 20783-1197
1	OSD	_	n m n amon
	OUSD(A&T)/ODDDR&E(R)	1	DIRECTOR
	R J TREW		US ARMY RESEARCH LAB
	THE PENTAGON		AMSRL CS AS (RECORDS MGMT)
	WASHINGTON DC 20301-7100		2800 POWDER MILL RD
			ADELPHI MD 20783-1145
1	DPTY CG FOR RDA		
	US ARMY MATERIEL CMD	3	DIRECTOR
	AMCRDA		US ARMY RESEARCH LAB
	5001 EISENHOWER AVE		AMSRL CI LL
	ALEXANDRIA VA 22333-0001		2800 POWDER MILL RD
	ALLEM NOTE TO THE PROPERTY OF		ADELPHI MD 20783-1145
1	INST FOR ADVNCD TCHNLGY		
•	THE UNIV OF TEXAS AT AUSTIN		
	PO BOX 202797		ABERDEEN PROVING GROUND
	AUSTIN TX 78720-2797		MODROLLIN THO VINC ORGOTA
	AUSTIN 1X 78720-2797	4	DIR USARL
	D.1001	-	
1	DARPA		AMSRL CI LP (BLDG 305)
	B KASPAR		
	3701 N FAIRFAX DR		
	ARLINGTON VA 22203-1714	•	
1	NAVAL SURFACE WARFARE CTR		
1			
	CODE B07 J PENNELLA		
	17320 DAHLGREN RD		
	BLDG 1470 RM 1101		
	DAHLGREN VA 22448-5100		
1	US MILITARY ACADEMY		
1	MATH SCI CTR OF EXCELLENCE		
	DEPT OF MATHEMATICAL SCI		
	MADN MATH		

THAYER HALL

WEST POINT NY 10996-1786

NO. OF COPIES	ORGANIZATION	NO. OF COPIES	ORGANIZATION
1	DIRECTOR US ARMY RESEARCH LAB AMSRL CP CA D SNIDER 2800 POWDER MILL RD ADELPHI MD 20783-1145	1	COMMANDER US ARMY MATERIEL CMD AMXMI INT 5001 EISENHOWER AVE ALEXANDRIA VA 22333-0001
1	DIRECTOR US ARMY RESEARCH LAB AMSRL OP SD TA 2800 POWDER MILL ROAD ADELPHI MD 20783-1145	2	COMMANDER US ARMY ARDEC AMSTA AR AE WW E BAKER J PEARSON PICATINNY ARSENAL NJ
3	DIRECTOR US ARMY RESEARCH LAB AMSRL OP SD TL 2800 POWDER MILL ROAD ADELPHI MD 20783-1145 DIRECTOR	1	O7806-5000  COMMANDER US ARMY ARDEC AMSTA AR TD C SPINELLI PICATINNY ARSENAL NJ
-	US ARMY RESEARCH LAB AMSRL OP SD TP 2800 POWDER MILL ROAD ADELPHI MD 20783-1145	1	07806-5000  COMMANDER US ARMY ARDEC AMSTA AR FSE
2	DIRECTOR US ARMY RESEARCH LAB AMSRL OP CI AD TECH PUB BR RECORDS MGMT ADMIN 2800 POWDER MILL ROAD ADELPHI MD 20783-1197	6	T GORA PICATINNY ARSENAL NJ  COMMANDER US ARMY ARDEC AMSTA AR CCH A W ANDREWS S MUSALLI
1	HQDA DAMI FIT NOLAN BLDG WASHINGTON DC 20310-1025 DIRECTOR		R CARR M LUCIANO E LOGSDEN T LOUZEIRO PICATINNY ARSENAL NJ 07806-5000
	DA OASARDA SARD SO 103 ARMY PENTAGON WASHINGTON DC 20310-0103	4	COMMANDER US ARMY ARDEC AMSTA AR CC G PAYNE
1	DEPUTY ASST SCY FOR R&T SARD TT RM 3EA79 THE PENTAGON WASHINGTON DC 20301-7100		J GEHBAUER C BAULIEU H OPAT PICATINNY ARSENAL NJ 07806-5000

1	COMMANDER US ARMY ARDEC AMSTA AR FSP A P KISATSKY PICATINNY ARSENAL NJ 07806-5000
	COMMANDER US ARMY ARDEC AMSTA AR CCH C H CHANIN S CHICO PICATINNY ARSENAL NJ 07806-5000
	COMMANDER US ARMY ARDEC AMSTA AR CCH B P DONADIA F DONLON P VALENTI
	C KNUTSON G EUSTICE S PATEL G WAGNECZ R SAYER F CHANG PICATINNY ARSENAL NJ 07806-5000
] ] ] ]	COMMANDER US ARMY ARDEC AMSTA AR CCL F PUZYCKI R MCHUGH D CONWAY E JAROSZEWSKI R SCHLENNER
1 (1 (1 (1 (1 (1 (1 (1 (1 (1 (1 (1 (1 (1	M CLUNE PICATINNY ARSENAL NJ 07806-5000  COMMANDER US ARMY ARDEC AMSTA AR QAC T D RIGOGLIOSO PICATINNY ARSENAL NJ 07806-5000
	2 9

## NO. OF COPIE ORGANIZATION

- 1 COMMANDER
  US ARMY ARDEC
  AMSTA AR SRE
  D YEE
  PICATINNY ARSENAL NJ
  07806-5000
- 1 COMMANDER
  US ARMY ARDEC
  AMSTA AR WET
  T SACHAR
  BLDG 172
  PICATINNY ARSENAL NJ
  07806-5000
- 1 COMMANDER
  US ARMY ARDEC
  SMCAR ASF
  PICATINNY ARSENAL NJ
  07806-5000
- 1 COMMANDER
  US ARMY ARDEC
  AMSTA AR WEL F
  INTELLIGENCE SPECIALIST
  M GUERRIERE
  PICATINNY ARSENAL NJ
  07806-5000
- 11 PROJECT MANAGER TANK MAIN ARMAMENT SYSTEMS SFAE GSSC TMA R MORRIS C KIMKER D GUZOWICZ E KOPACZ R ROESER R DARCY R MCDANOLDS L D ULISSE C ROLLER J MCGREEN **B PATTER** PICATINNY ARSENAL NJ 07806-5000

## NO. OF COPIES ORGANIZATION

- 2 PEO FIELD ARTILLERY SYSTEMS SFAE FAS PM H GOLDMAN T MCWILLIAMS PICATINNY ARSENAL NJ 07806-5000
- 6 PM SADARM
  SFAE GCSS SD
  COL B ELLIS
  M DEVINE
  R KOWALSKI
  W DEMASSI
  J PRITCHARD
  S HROWNAK
  PICATINNY ARSENAL NJ
  07806-5000
- 1 COMMANDER
  US ARMY ARDEC
  PRODUCTION BASE
  MODERN ACTY
  AMSMC PBM K
  PICATINNY ARSENAL NJ
  07806-5000
- 3 COMMANDER
  U S ARMY TACOM
  PM TACTICAL VEHICLES
  SFAE TVL
  SFAE TVM
  SFAE TVH
  6501 ELEVEN MILE RD
  WARREN MI 48397-5000
- U S ARMY TACOM
  PM ABRAMS
  SFAE ASM AB
  6501 ELEVEN MILE RD
  WARREN MI 48397-5000
- 1 COMMANDER
  U S ARMY TACOM
  PM BFVS
  SFAE ASM BV
  6501 ELEVEN MILE RD
  WARREN MI 48397-5000

NO. OF COPIES	ORGANIZATION	NO. OF COPIES	ORGANIZATION
1	COMMANDER U S ARMY TACOM PM AFAS SFAE ASM AF 6501 ELEVEN MILE RD WARREN MI 48397-5000	1	COMMANDER U S ARMY TACOM PM GROUND SYSTEMS INTEGRATION SFAE GCSS W GSI R LABATILLE 6501 ELEVEN MILE RD
	COMMANDER U S ARMY TACOM PM SURV SYS SFAE ASM SS T DEAN SFAE GCSS W GSI M D COCHRAN 6501 ELEVEN MILE RD WARREN MI 48397-5000	1	WARREN MI 48397-5000  COMMANDER U S ARMY TACOM CHIEF ABRAMS TESTING SFAE GCSS W AB QT T KRASKIEWICZ 6501 ELEVEN MILE RD WARREN MI 48397-5000
1	COMMANDER U S ARMY TACOM PM RDT&E SFAE GCSS W AB J GODELL	1	COMMANDER US ARMY TACOM AMSTA SF WARREN MI 48397-5000
1	6501 ELEVEN MILE RD WARREN MI 48397-5000  COMMANDER U S ARMY TACOM PM SURVIVABLE SYSTEMS SFAE GCSS W GSI H	1	COMMANDER SMCWV QAE Q B VANINA BLDG 44 WATERVLIET ARSENAL WATERVLIET NY 12189-4050
	M RYZYI 6501 ELEVEN MILE RD WARREN MI 48397-5000	14	COMMANDER US ARMY TACOM ASMTA TR R J CHAPIN
1	COMMANDER U S ARMY TACOM PM BFV SFAE GCSS W BV S DAVIS 6501 ELEVEN MILE RD WARREN MI 48397-5000		R MCCLELLAND D THOMAS J BENNETT D HANSEN AMSTA JSK S GOODMAN J FLORENCE K IYER
1	COMMANDER U S ARMY TACOM PM LIGHT TACTICAL VEHICLES AMSTA TR S AJ J MILLS MS 209 6501 ELEVEN MILE RD WARREN MI 48397-5000		J THOMSON AMSTA TR D D OSTBERG L HINOJOSA B RAJU AMSTA CS SF H HUTCHINSON F SCHWARZ WARREN MI 48397-5000

NO. OF COPIES	ORGANIZATION	NO. OF COPIES	ORGANIZATION
1	COMMANDER SMCWV SPM T MCCLOSKEY BLDG 253 WATERVLIET ARSENAL WATERVLIET NY 12189-4050	4	DIRECTOR US ARMY CECOM NIGHT VISION AND ELECTRONIC SENSORS DIRECTORATE AMSEL RD NV CM CCD R ADAMS R MCLEAN
10	BENET LABORATORIES AMSTA AR CCB R FISCELLA G D ANDREA M SCAVULO G SPENCER		A YINGST AMSEL RD NV VISP E JACOBS 10221 BURBECK RD FT BELVOIR VA 22060-5806
	P WHEELER K MINER J VASILAKIS G FRIAR R HASENBEIN	2	CDR USA AMCOM AVIATION APPLIED TECH DIR J SCHUCK FT EUSTIS VA 23604-5577
	SMCAR CCB R S SOPOK WATERVLIET NY 12189	1	U S ARMY CRREL P DUTTA 72 LYME RD HANOVER NH 03755
2	TSM ABRAMS ATZK TS S JABURG W MEINSHAUSEN FT KNOX KY 40121	1	US ARMY CERL R LAMPO 2902 NEWMARK DR CHAMPAIGN IL 61822
3	ARMOR SCHOOL ATTN ATZK TD R BAUEN J BERG A POMEY FT KNOX KY 40121	2	U S ARMY CORP OF ENGINEERS CERD C T LIU CEW ET T TAN 20 MASS AVE NW WASHINGTON DC 20314
2	HQ IOC TANK AMMO TEAM AMSIO SMT R CRAWFORD W HARRIS ROCK ISLAND IL 61299-6000	10	DIRECTOR US ARMY NATL GRND INTEL CTR D LEITER S EITELMAN M HOLTUS M WOLFE S MINGLEDORF
1	DIRECTOR U S ARMY AMCOM SFAE AV RAM TV D CALDWELL BUILDING 5300 REDSTONE ARSENAL AL 35898		H C ARDLEIGH J GASTON W GSTATTENBAUER R WARNER J CRIDER 220 SEVENTH STREET NE CHARLOTTESVILLE VA 22091

NO. OF COPIES	ORGANIZATION	NO. OF COPIES	<u>ORGANIZATION</u>
6	US ARMY SBCCOM SOLDIER SYSTEMS CENTER BALLISTICS TEAM J WARD MARINE CORPS TEAM J MACKIEWICZ	1	COMMANDANT U S ARMY FIELD ARTILLERY CTR AT FT SILL ATFS CD LTC BUMGARNER FT SILL OK 73503 5600
	BUS AREA ADVOCACY TEAM W HASKELL SSCNC WST W NYKVIST T MERRILL	1	CHIEF USAIC LTC T J CUMMINGS ATZB COM FT BENNING GA 31905-5800
1	S BEAUDOIN KANSAS ST NATICK MA 01760-5019 US ARMY COLD	1	NAVAL AIR SYSTEMS CMD J THOMPSON 48142 SHAW RD UNIT 5 PATUXENT RIVER MD 20670
ı	REGIONS RSCH & ENGRNG LAB P DUTTA 72 LYME RD	1	NAVAL SURFACE WARFARE CTR DAHLGREN DIV CODE G06 DAHLGREN VA 22448
	HANOVER NH 03755	1	NAVAL SURFACE WARFARE CTR TECH LIBRARY CODE 323
1	SYSTEM MANAGER ABRAMS BLDG 1002 RM 110 ATZK TS LTC J H NUNN		17320 DAHLGREN RD DAHLGREN VA 22448
9	FT KNOX KY 40121  US ARMY RESEARCH OFFICE A CROWSON J CHANDRA	. 3	NAVAL RESEARCH LAB I WOLOCK CODE 6383 R BADALIANCE CODE 6304 L GAUSE WASHINGTON DC 20375
	H EVERETT J PRATER R SINGLETON G ANDERSON D STEPP D KISEROW	1	NAVAL SURFACE WARFARE CTR CRANE DIVISION M JOHNSON CODE 20H4 LOUISVILLE KY 40214-5245
	J CHANG PO BOX 12211 RESEARCH TRIANGLE PARK NC 27709-2211	2	COMMANDER NAVAL SURFACE WARFARE CTR CADEROCK DIVISION R PETERSON CODE 2020 M CRITCHFIELD CODE 1730
1	DIRECTORATE OF CMBT DEVELOPMENT	•	BETHESDA MD 20084
	C KJORO 320 ENGINEER LOOP STE 141 FT LEONARD WOOD MO 65473-8929	2	NAVAL SURFACE WARFARE CTR U SORATHIA C WILLIAMS CD 6551 9500 MACARTHUR BLVD WEST BETHESDA MD 20817

NO. OF COPIES	ORGANIZATION	NO. OF COPIES	ORGANIZATION
1	DAVID TAYLOR RESEARCH CTR SHIP STRUCTURES & PROTECTION DEPARTMENT CODE 1702 J CORRADO BETHESDA MD 20084	1	NAVSEA OJRI PEO DD21 PMS500 G CAMPONESCHI 2351 JEFFERSON DAVIS HWY ARLINGTON VA 22242-5165
2	DAVID TAYLOR RESEARCH CTR R ROCKWELL W PHYILLAIER BETHESDA MD 20054-5000	1	EXPEDITIONARY WARFARE DIV N85 F SHOUP 2000 NAVY PENTAGON WASHINGTON DC 20350-2000
1	OFFICE OF NAVAL RESEARCH D SIEGEL CODE 351 800 N QUINCY ST ARLINGTON VA 22217-5660	1	AFRL MLBC 2941 P STREET RM 136 WRIGHT PATTERSON AFB OH 45433-7750
8	NAVAL SURFACE WARFARE CTR J FRANCIS CODE G30 D WILSON CODE G32 R D COOPER CODE G32 J FRAYSSE CODE G33 E ROWE CODE G33	1	AFRL MLSS R THOMSON 2179 12TH STREET RM 122 WRIGHT PATTERSON AFB OH 45433-7718
	T DURAN CODE G33 L DE SIMONE CODE G33 R HUBBARD CODE G33 DAHLGREN VA 22448	2	AFRL F ABRAMS J BROWN BLDG 653
1	NAVAL SEA SYSTEMS CMD D LIESE 2531 JEFFERSON DAVIS HIGHWAY ARLINGTON VA 22242-5160	1	2977 P STREET STE 6 WRIGHT PATTERSON AFB OH 45433-7739 AFRL MLS OL
1	NAVAL SURFACE WARFARE M LACY CODE B02 17320 DAHLGREN RD DAHLGREN VA 22448	1	7278 4TH STREET BLDG 100 BAY D L COULTER HILL AFB UT 84056-5205
1	OFFICE OF NAVAL RES J KELLY 800 NORTH QUINCEY ST ARLINGTON VA 22217-5000	1	OSD JOINT CCD TEST FORCE OSD JCCD R WILLIAMS 3909 HALLS FERRY RD VICKSBURG MS 29180-6199
2	NAVAL SURFACE WARFARE CTR CARDEROCK DIVISION R CRANE CODE 2802 C WILLIAMS CODE 6553 3A LEGGETT CIR BETHESDA MD 20054-5000	1	DEFENSE NUCLEAR AGENCY INNOVATIVE CONCEPTS DIV R ROHR 6801 TELEGRAPH RD ALEXANDRIA VA 22310-3398

NO. OF COPIES	ORGANIZATION	NO. OF <u>COPIES</u>	<u>ORGANIZATION</u>
1	WATERWAYS EXPERIMENT	5	DIRECTOR
	D SCOTT		LAWRENCE LIVERMORE
	3909 HALLS FERRY RD SC C		NATL LAB
	VICKSBURG MS 39180		R CHRISTENSEN
			S DETERESA
3	DARPA		F MAGNESS
	M VANFOSSEN		M FINGER MS 313 M MURPHY L 282
	S WAX L CHRISTODOULOU		PO BOX 808
	3701 N FAIRFAX DR		LIVERMORE CA 94550
	ARLINGTON VA 22203-1714		LIVERWORD CA 94330
	AUDITOR VA 22205-1714	7	NIST
2	SERDP PROGRAM OFC PM P2	•	R PARNAS
_	C PELLERIN		J DUNKERS
	B SMITH		M VANLANDINGHAM MS 8621
	901 N STUART ST SUITE 303		J CHIN MS 8621
	ARLINGTON VA 22203		D HUNSTON MS 8543
			J MARTIN MS 8621
1	FAA		D DUTHINH MS 8611
	MIL HDBK 17 CHAIR		100 BUREAU DR
	L ILCEWICZ 1601 LIND AVE SW		GAITHERSBURG MD 20899
	ANM 115N	1	OAK RIDGE NATL LAB
	RENTON VA 98055	1	C EBERLE MS 8048
	ALIVION VA 70033		PO BOX 2009
2	FAA TECH CENTER		OAK RIDGE TN 37831
	D OPLINGER AAR 431		
	P SHYPRYKEVICH AAR 431	1	OAK RIDGE NATL LAB
	ATLANTIC CITY NJ 08405		C D WARREN MS 8039
			PO BOX 2009
1	OFC OF ENVIRONMENTAL MGMT		OAK RIDGE TN 37922
	U S DEPT OF ENERGY		
	P RITZCOVAN	4	DIRECTOR
	19901 GERMANTOWN RD GERMANTOWN MD 20874-1928		SANDIA NATL LABS APPLIED MECHANICS DEPT
	GERMAN 10 WIN MID 208/4-1928		DIVISION 8241
1	LOS ALAMOS NATL LAB		W KAWAHARA
	F ADDESSIO		K PERANO
	MS B216		D DAWSON
	PO BOX 1633		P NIELAN
	LOS ALAMOS NM 87545		PO BOX 969
			LIVERMORE CA 94550-0096
1	OAK RIDGE NATL LAB		
	R M DAVIS	1	LAWRENCE LIVERMORE
	PO BOX 2008		NATIONAL LAB
	OAK RIDGE TN 37831-6195		M MURPHY
			PO BOX 808 L 282
			LIVERMORE CA 94550

NO. OF COPIES	ORGANIZATION	NO. OF COPIES	ORGANIZATION
3	NASA LANGLEY RESEARCH CTR MS 266 AMSRL VS W ELBER	1	GRAPHITE MASTERS INC J WILLIS 3815 MEDFORD ST LOS ANGELES CA 90063-1900
	F BARTLETT JR G FARLEY HAMPTON VA 23681-0001	1	ADVANCED GLASS FIBER YARNS T COLLINS 281 SPRING RUN LN STE A
1	NASA LANGLEY RESEARCH CTR T GATES MS 188E	•	DOWNINGTON PA 19335  COMPOSITE MATERIALS INC
	HAMPTON VA 23661-3400	1	D SHORTT 19105 63 AVE NE
1	USDOT FEDERAL RAILROAD RDV 31 M FATEH WASHINGTON DC 20590		PO BOX 25 ARLINGTON WA 98223
1	DOT FHWA J SCALZI 400 SEVENTH ST SW 3203 HNG 32	. 1	COMPOSITE MATERIALS INC R HOLLAND 11 JEWEL COURT ORINDA CA 94563
	WASHINGTON DC 20590	1	COMPOSITE MATERIALS INC
1	FHWA E MUNLEY 6300 GEORGETOWN PIKE MCLEAN VA 22101		14530 S ANSON AVE SANTA FE SPRINGS CA 90670
1	CENTRAL INTELLIGENCE AGENCY OTI WDAG GT W L WALTMAN PO BOX 1925 WASHINGTON DC 20505	2	COMPOSIX D BLAKE L DIXON 120 O NEILL DR HEBRUN OHIO 43025
1	MARINE CORPS INTEL ACTY D KOSITZKE 3300 RUSSELL RD SUITE 250 QUANTICO VA 22134-5011	4	CYTEC FIBERITE R DUNNE D KOHLI M GILLIO R MAYHEW 1300 REVOLUTION ST HAVRE DE GRACE MD 21078
1	NATL GRND INTELLIGENCE CTR DIRECTOR IANG TMT 220 SEVENTH ET NE CHARLOTTESVILLE VA 22902-5396	2	SIMULA J COLTMAN R HUYETT 10016 S 51ST ST
	DIRECTOR DEFENSE INTELLIGENCE AGENCY TA 5 K CRELLING WASHINGTON DC 20310	1	PHOENIX AZ 85044  SIOUX MFG B KRIEL PO BOX 400 FT TOTTEN ND 58335

NO. OF COPIES	ORGANIZATION	NO. OF COPIES	<u>ORGANIZATION</u>
2	PROTECTION MATERIALS INC M MILLER F CRILLEY 14000 NW 58 CT MIAMI LAKES FL 33014	1	BATTELLE C R HARGREAVES 505 KING AVE COLUMBUS OH 43201-2681
3	FOSTER MILLER J J GASSNER M ROYLANCE W ZUKAS 195 BEAR HILL RD WALTHAM MA 02354-1196	2	BATTELLE NATICK OPERATIONS J CONNORS B HALPIN 209 W CENTRAL ST STE 302 NATICK MA 01760
1	ROM DEVELOPMENT CORP R O MEARA 136 SWINEBURNE ROW BRICK MARKET PLACE NEWPORT RI 02840	1	BATTELLE NW DOE PNNL T HALL MS K231 BATTELLE BLVD RICHLAND WA 99352
2	TEXTRON SYSTEMS T FOLTZ M TREASURE 201 LOWELL ST WILMINGTON MA 08870-2941	3	PACIFIC NORTHWEST LAB M SMITH G VAN ARSDALE R SHIPPELL PO BOX 999 RICHLAND WA 99352
	JPS GLASS L CARTER PO BOX 260 SLATER RD SLATER SC 29683	1	ARMTEC DEFENSE PRODUCTS S DYER 85 901 AVE 53 PO BOX 848 COACHELLA CA 92236
	O GARA HESS & EISENHARDT M GILLESPIE 9113 LESAINT DR FAIRFIELD OH 45014		ADVANCED COMPOSITE MATLS CORP P HOOD J RHODES 1525 S BUNCOMBE RD GREER SC 29651-9208
	MILLIKEN RESEARCH CORP H KUHN M MACLEOD PO BOX 1926 SPARTANBURG SC 29303	2	GLCC INC J RAY M BRADLEY 103 TRADE ZONE DR
]	CONNEAUGHT INDUSTRIES INC I SANTOS PO BOX 1425 COVENTRY RI 02816	2	STE 26C WEST COLUMBIA SC 29170  AMOCO PERFORMANCE PRODUCTS M MICHNO JR J BANISAUKAS 4500 MCGINNIS FERRY RD ALPHARETTA GA 30202-3944

NO. OF COPIES	ORGANIZATION	NO. OF COPIES	ORGANIZATION
1	SAIC M PALMER 2109 AIR PARK RD S E	1	PROJECTILE TECHNOLOGY INC 515 GILES ST HAVRE DE GRACE MD 21078
	ALBUQUERQUE NM 87106	1	CUSTOM ANALYTICAL ENG SYS INC
1	SAIC ATTN G CHRYSSOMALLIS 3800 W 80TH ST STE 1090 BLOOMINGTON MN 55431		A ALEXANDER 13000 TENSOR LN NE FLINTSTONE MD 21530
1	AAI CORPORATION DR T G STASTNY PO BOX 126 HUNT VALLEY MD 21030-0126	2	LORAL VOUGHT SYSTEMS G JACKSON K COOK 1701 W MARSHALL DR GRAND PRAIRIE TX 75051
1	JOHN HEBERT PO BOX 1072 HUNT VALLEY MD 21030-0126	5	AEROJET GEN CORP D PILLASCH T COULTER
12	ALLIANT TECHSYSTEMS INC C CANDLAND C AAKHUS R BECKER B SEE N VLAHAKUS		C FLYNN D RUBAREZUL M GREINER 1100 WEST HOLLYVALE ST AZUSA CA 91702-0296
	R DOHRN S HAGLUND D FISHER W WORRELL R COPENHAFER M HISSONG	. 3	HEXCEL INC R BOE F POLICELLI J POESCH PO BOX 98 MAGNA UT 84044
3	D KAMDAR 600 2ND ST NE HOPKINS MN 55343-8367  ALLIANT TECHSYSTEMS INC J CONDON	3	HERCULES INC G KUEBELER J VERMEYCHUK B MANDERVILLE JR HERCULES PLAZA WILMINGTON DE 19894
	E LYNAM J GERHARD WV01 16 STATE RT 956 PO BOX 210 ROCKET CENTER WV 26726-0210	1	BRIGS COMPANY J BACKOFEN 2668 PETERBOROUGH ST HERDON VA 22071-2443
1	APPLIED COMPOSITES W GRISCH 333 NORTH SIXTH ST ST CHARLES IL 60174	1	ZERNOW TECHNICAL SERVICES L ZERNOW 425 W BONITA AVE STE 208 SAN DIMAS CA 91773

NO. OF COPIES	ORGANIZATION	NO. OF COPIES	ORGANIZATION
2	OLIN CORPORATION FLINCHBAUGH DIV E STEINER B STEWART PO BOX 127	1	BOEING R BOHLMANN PO BOX 516 MC 5021322 ST LOUIS MO 63166-0516
	RED LION PA 17356	2	BOEING DEFENSE AND SPACE GRP
1	OLIN CORPORATION L WHITMORE 10101 9TH ST NORTH ST PETERSBURG FL 33702		W HAMMOND J RUSSELL S 4X55 PO BOX 3707 SEATTLE WA 98124-2207
1	DOW UT	2	DOEDIG DOTODOD AFT
5	S TIDRICK 15 STERLING DR WALLINGFORD CT 06492 SIKORSKY AIRCRAFT G JACARUSO	2	BOEING ROTORCRAFT P MINGURT P HANDEL 800 B PUTNAM BLVD WALLINGFORD PA 19086
	T CARSTENSAN B KAY S GARBO M S S330A J ADELMANN 6900 MAIN ST PO BOX 9729 STRATFORD CT 06497-9729	1	BOEING DOUGLAS PRODUCTS DIV L J HART SMITH 3855 LAKEWOOD BLVD D800 0019 LONG BEACH CA 90846-0001
1	PRATT & WHITNEY D HAMBRICK 400 MAIN ST MS 114 37 EAST HARTFORD CT 06108	1	LOCKHEED MARTIN S REEVE 8650 COBB DR D 73 62 MZ 0648 MARIETTA GA 30063-0648
1	AEROSPACE CORP G HAWKINS M4 945 2350 E EL SEGUNDO BLVD EL SEGUNDO CA 90245	1	LOCKHEED MARTIN SKUNK WORKS D FORTNEY 1011 LOCKHEED WAY PALMDALE CA 93599-2502
2	CYTEC FIBERITE M LIN W WEB 1440 N KRAEMER BLVD ANAHEIM CA 92806	1	LOCKHEED MARTIN R FIELDS 1195 IRWIN CT WINTER SPRINGS FL 32708
1	HEXCEL T BITZER 11711 DUBLIN BLVD DUBLIN CA 94568	1	MATERIALS SCIENCES CORP B W ROSEN 500 OFFICE CENTER DR STE 250 FORT WASHINGTON PA 19034

NO. OF COPIES	ORGANIZATION	NO. OF <u>COPIES</u>	ORGANIZATION
1	NORTHRUP GRUMMAN CORP ELECTRONIC SENSORS & SYSTEMS DIV E SCHOCH 1745A WEST NURSERY RD MAILSTOP V 16 LINTHICUM MD 21090	2	GENERAL DYNAMICS LAND SYSTEMS D REES M PASIK PO BOX 2074 WARREN MI 48090-2074
2	NORTHROP GRUMMAN ENVIRONMENTAL PROGRAMS R OSTERMAN A YEN 8900 E WASHINGTON BLVD PICO RIVERA CA 90660	1	GENERAL DYNAMICS LAND SYSTEMS DIVISION D BARTLE PO BOX 1901 WARREN MI 48090 GENERAL DYNAMICS
1	UNITED DEFENSE LP PO BOX 359 D MARTIN SANTA CLARA CA 95052		LAND SYSTEMS MUSKEGON OPERATIONS W SOMMERS JR 76 GETTY ST MUSKEGON MI 49442
2	UNITED DEFENSE LP PO BOX 58123 G THOMAS SANTA CLARA CA 95052 UNITED DEFENSE LP	1	GENERAL DYNAMICS AMPHIBIOUS SYS SURVIVABILITY LEAD G WALKER 991 ANNAPOLIS WAY WOODBRIDGE VA 22191
	MAIL DROP M53 R BARRETT V HORVATICH 328 W BROKAW RD SANTA CLARA CA 95052-0359	5	INSTITUTE FOR ADVANCED TECH T KIEHNE H FAIR P SULLIVAN
3	UNITED DEFENSE LP GROUND SYSTEMS DIVISION M PEDRAZZI MAIL DROP N09 A LEE MAIL DROP N11 M MACLEAN MAIL DROP N06 1205 COLEMAN AVE	2	W REINECKE I MCNAB 4030 2 W BRAKER LN AUSTIN TX 78759 CIVIL ENGR RSCH FOUNDATION
4	SANTA CLARA CA 95052 UNITED DEFENSE LP	2	H BERNSTEIN PRESIDENT R BELLE 1015 15TH ST NW STE 600 WASHINGTON DC 20005
	4800 EAST RIVER RD R BRYNSVOLD P JANKE MS170 T GIOVANETTI MS236 B VAN WYK MS389 MINNEAPOLIS MN 55421-1498	1	ARROW TECH ASSO 1233 SHELBURNE RD STE D 8 SOUTH BURLINGTON VT 05403-7700

NO. OF COPIES	ORGANIZATION	NO. OF COPIES	ORGANIZATION
1	CONSULTANT R EICHELBERGER 409 W CATHERINE ST BEL AIR MD 21014-3613	1	UNIVERSITY OF UTAH DEPT OF MECH & INDUSTRIAL ENGR S SWANSON SALT LAKE CITY UT 84112
1	UCLA MANE DEPT ENGR IV H THOMAS HAHN LOS ANGELES CA 90024-1597	2	PENNSYLVANIA STATE UNIV R MCNITT C BAKIS
2	U OF DAYTON RESEARCH INSTUTE RAN Y KIM AJIT K ROY		227 HAMMOND BLDG UNIVERSITY PARK PA 16802
1	300 COLLEGE PARK AVE DAYTON OH 45469-0168 MIT	1	PENNSYLVANIA STATE UNIV RENATA S ENGEL 245 HAMMOND BLDG UNIVERSITY PARK PA 16801
•	P LAGACE 77 MASS AVE CAMBRIDGE MA 01887	1	PURDUE UNIVERSITY SCHOOL OF AERO & ASTRO
1	IIT RESEARCH CENTER D ROSE 201 MILL ST	1	C T SUN W LAFAYETTE IN 47907-1282 STANFORD UNIVERSITY
1	ROME NY 13440-6916 GEORGIA TECH	•	DEPARTMENT OF AERONAUTICS AND AEROBALLISTICS DURANT BUILDING
	RESEARCH INSTITUTE GEORGIA INSTITUTE OF TECHNOLOGY		S TSAI STANFORD CA 94305
1	P FRIEDERICH ATLANTA GA 30392 MICHIGAN ST UNIVERSITY	1	UNIVERSITY OF DAYTON J M WHITNEY COLLEGE PARK AVE DAYTON OH 45469-0240
1	R AVERILL 3515 EB MSM DEPT EAST LANSING MI 48824-1226	7	UNIVERSITY OF DELAWARE CTR FOR COMPOSITE
1	UNIVERSITY OF KENTUCKY LYNN PENN 763 ANDERSON HALL		MATERIALS J GILLESPIE M SANTARE G DAL MESE
1	763 ANDERSON HALL LEXINGTON KY 40506-0046 UNIVERSITY OF WYOMING		G PALMESE S YARLAGADDA S ADVANI D HEIDER
. <b>^</b>	D ADAMS PO BOX 3295 LARAMIE WY 82071		D KUKICH 201 SPENCER LABORATORY NEWARK DE 19716

NO. OF COPIES	ORGANIZATION	NO. OF COPIES	<u>ORGANIZATION</u>	
1	UNIVERSITY OF ILLINOIS AT URBANA CHAMPAIGN		ABERDEEN PROVING GROUND	
	NATL CENTER FOR COMPOSITE	1	COMMANDER	
	MATERIALS RESEARCH 216 TALBOT LABORATORY		US ARMY MATERIEL SYS ANALYSIS	
	JECONOMY		P DIETZ	
	104 S WRIGHT ST		392 HOPKINS RD	
	URBANA IL 61801		AMXSY TD	
			APG MD 21005-5071	
3	THE UNIVERSITY OF TEXAS	_	DIDECTION .	
	AT AUSTIN	1	DIRECTOR	
	CENTER FOR ELECTROMECHANICS		US ARMY RESEARCH LAB AMSRL OP AP L	
	J PRICE A WALLS		APG MD 21005 5066	
	J KITZMILLER			
	10100 BURNET RD	115	DIR USARL	
	AUSTIN TX 78758-4497		AMSRL CI	
			AMSRL CI H	
3	VA POLYTECHNICAL INSTITUTE		W STUREK	
	& STATE UNIVERSITY	AMSRL CI S		
	DEPT OF ESM		A MARK	
	M W HYER		AMSRL CS IO FI M ADAMSON	
	K REIFSNIDER R JONES		AMSRL SL B	
	BLACKSBURG VA 24061-0219		J SMITH	
	BLACKSBOKG VII 24001 0217		AMSRL SL BA	
1	NORTH CAROLINA STATE		AMSRL SL BL	
	UNIVERSITY		D BELY	
	CIVIL ENGINEERING DEPT		RHENRY	
	WRASDORF		AMSRL SL BG	
	PO BOX 7908		A YOUNG AMSRL SL I	
	RALEIGH NC 27696-7908		AMSRL WM B	
1	UNIVERSITY OF MARYLAND		A HORST	
	DEPT OF AEROSPACE ENGINEERING		E SCHMIDT	
	ANTHONY J VIZZINI		AMSRL WM BA	
	COLLEGE PARK MD 20742		W D AMICO	
			F BRANDON AMSRL WM BC	
1	DREXEL UNIVERSITY		P PLOSTINS	
	ALBERT S D WANG 32ND AND CHESTNUT STREETS		DLYON	
	PHILADELPHIA PA 19104		J NEWILL	
			S WILKERSON	
1	SOUTHWEST RSCH INSTITUTE		A ZIELINSKI	
	ENGR & MATL SCIENCES DIV		AMSRL WM BD	
	J RIEGEL		B FORCH	
	6220 CULEBRA RD		R FIFER R PESCE RODRIGUEZ	
	PO DRAWER 28510		B RICE	
	SAN ANTONIO TX 78228-0510		D RICH	

NO. OF

COPIES ORGANIZATION

#### ABERDEEN PROVING GROUND (CONT)

AMSRL WM MB

ABERDEEN PROVING GROUND (CONT)

**E RIGAS** 

J SANDS

D SPAGNUOLO

W SPURGEON

J TZENG

E WETZEL

A ABRAHAMIAN

M BERMAN A FRYDMAN

TLI

W MCINTOSH E SZYMANSKI

AMRSL WM MC

J BEATTY

**J SWAB** 

**E CHIN** 

J MONTGOMERY

A WERESCZCAK

J LASALVIA

J WELLS

AMSRL WM MD

W ROY

S WALSH

AMSRL WM T

**B BURNS** 

AMSRL WM TA

W GILLICH

T HAVEL

J RUNYEON

**M BURKINS** 

E HORWATH

**B GOOCH** 

W BRUCHEY

AMSRL WM TC

R COATES

AMSRL WM TD

A DAS GUPTA

T HADUCH

T MOYNIHAN

F GREGORY

A RAJENDRAN

M RAFTENBERG

**M BOTELER** 

T WEERASOORIYA D DANDEKAR

A DIETRICH

AMSRL WM BE

G WREN

**CLEVERITT** 

D KOOKER

AMSRL WM BR

C SHOEMAKER

J BORNSTEIN

AMSRL WM M

D VIECHNICKI

**G HAGNAUER** 

J MCCAULEY

**B TANNER** 

AMSRL WM MA

R SHUFORD

P TOUCHET

N BECK TAN

**DFLANAGAN** 

L GHIORSE

**D HARRIS** 

S MCKNIGHT

P MOY

**S NGYUEN** 

**PPATTERSON** 

**G RODRIGUEZ** 

A TEETS R YIN

AMSRL WM MB

**B FINK** 

J BENDER

T BLANAS

T BOGETTI

R BOSSOLI

L BURTON K BOYD

S CORNELISON

P DEHMER

R DOOLEY

W DRYSDALE

**G GAZONAS** 

**S GHIORSE** 

D GRANVILLE

D HOPKINS

C HOPPEL

D HENRY

R KASTE

**M KLUSEWITZ** 

**M LEADORE** 

R LIEB

NO. OF

#### COPIES ORGANIZATION

### ABERDEEN PROVING GROUND (CONT)

AMSRL WM TE

A NIILER

J POWELL

AMSRL SS SD

H WALLACE

AMSRL SS SE R

R CHASE

AMSRL SS SE DS

R REYZER

R ATKINSON

AMSRL SE L

R WEINRAUB

J DESMOND

D WOODBURY

## NO. OF COPIE ORGANIZATION

- 1 R MARTIN
  MERL
  LTD
  TAMWORTH RD
  HERTFORD SG13 7DG
  UK
- 1 PW LAY
  SMC SCOTLAND
  DERA ROSYTH
  ROSYTH ROYAL DOCKYARD
  DUNFERMLINE FIFE KY 11 2XR
  UK
- 1 T GOTTESMAN
  CIVIL AVIATION ADMINSTRATION
  PO BOX 8
  BEN GURION INTERNL AIRPORT
  LOD 70150 ISREAL
- 1 S ANDRE
  AEROSPATIALE
  A BTE CC RTE MD132
  316 ROUTE DE BAYONNE
  TOULOUSE 31060
  FRANCE
- 1 J BAUER
  DAIMLER BENZ AEROSPACE
  D 81663 MUNCHEN
  MUNICH
  GERMANY
- 3 DRA FORT HALSTEAD
  PETER N JONES
  DAVID SCOTT
  MIKE HINTON
  SEVEN OAKS KENT TN 147BP
  UNITED KINGDOM
- 1 MR FRANCOIS LESAGE
  DEFENSE RESEARCH ESTAB
  VALCARTIER
  PO BOX 8800
  COURCELETTE QUEBEC COA
  IRO CANADA

## NO. OF COPIES ORGANIZATION

- 2 ROYAL MILITARY COLLEGE OF SCIENCE SHRIVENHAM D BULMAN B LAWTON SWINDON WILTS SN6 8LA UNITED KINGDOM
- 1 SWISS FEDERAL ARMAMENTS WKS WALTER LANZ ALLMENDSTRASSE 86 3602 THUN SWITZERLAND
- 1 PROFESSOR SOL BODNER
  ISRAEL INSTITUTE OF
  TECHNOLOGY
  FACULTY OF MECHANICAL ENGR
  HAIFA 3200 ISRAEL
- DSTO ATERIALS RESEARCH LAB
  DR NORBERT BURMAN NAVAL
  PLATFORM VULNERABILITY SHIP
  STRUCTURES & MATERIALS DIV
  PO BOX 50
  ASCOT VALE VICTORIA
  AUSTRALIA 3032
- PROFESSOR EDWARD CELENS
  ECOLE ROYAL MILITAIRE
  AVE DE LA RENAISSANCE 30
  1040 BRUXELLE
  BELGIQUE
- 1 DEF RES ESTABLISHMENT
  VALCARTIER
  ALAIN DUPUIS
  2459 BOULEVARD PIE XI NORTH
  VALCARTIER QUEBEC
  CANADA
  PO BOX 8800 COURCELETTE
  GOA IRO QUEBEC CANADA

### NO. OF COPIES ORGANIZATION

- 1 INSTITUT FRANCO ALLEMAND DE RECHERCHES DE SANIT LOUIS DE MARC GIRAUD RUE DU GENERAL CASSAGNOU BOITE POSTALE 34 F 68301 SAINT LOUIS CEDEX FRANCE
- J MANSONECOLE POLYTECHDMX LTCCH 1015 LAUSANNE SWITZERLAND
- 1 TNO PRINS MAURITS LAB
  DR ROB IJSSELSTEIN
  LANGE KLEIWEG 137
  PO BOX 45
  2280 AA RIJSWIJK
  THE NETHERLANDS
- 2 FOA NAT L DEFENSE
  RESEARCH ESTAB
  DR BO JANZON
  R HOLMLIN
  DIR DEPT OF WEAPONS &
  PROTECTION
  S 172 90 STOCKHOLM
  SWEDEN
- 2 DEFENSE TECH & PROC AGENCY GRND MR I CREWTHER GENERAL HERZOG HAUS 3602 THUN SWITZERLAND
- 1 MINISTRY OF DEFENCE RAFAEL DR MEIR MAYSELESS ARMAMENT DEVELOPMENT AUTH PO BOX 2250 HAIFA 31021 ISRAEL
- 1 DR AKE PERSSON DYNAMEC RESEARCH AB PARADISGRND 7 S 151 36 SODERTALJE SWEDEN

# NO. OF COPIES ORGANIZATION

- 1 ERNST MACH INSTITUT EMI DIRECTOR HAUPTSTRASSE 18 79576 WEIL AM RHEIN GERMANY
- 1 ERNST MACH INSTITUT EMI DR ALOIS STILP ECKERSTRASSE 4 7800 FREIBURG GERMANY
- 1 DR IR HANS PASMAN
  TNO DEFENSE RESEARCH
  POSTBUS 6006
  2600 JA DELFT
  THE NETHERLANDS
- 1 DR BITAN HIRSCH TACHKEMONY ST 6 NETAMUA 42611 ISRAEL
- 1 PROF DR MANFRED HELD DEUTSCHE AEROSPACE AG DYNAMICS SYSTEMS PO BOX 1340 D 86523 SCHROBENHAUSEN GERMANY

### Form Approved REPORT DOCUMENTATION PAGE OMB No. 0704-0188 Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for information Operations and Reports, 1215 Jefferson Davis Highway, Suits 1204, Arington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project(0704-0188), Washington, DC 20503. ork Reduction Project(0704-0188), Washington, DC 20503 3. REPORT TYPE AND DATES COVERED 2. REPORT DATE 1. AGENCY USE ONLY (Leave blank) Final, Mar 95 - Jan 96 June 2000 5. FUNDING NUMBERS 4. TITLE AND SUBTITLE An Evanescent Wave Fluorescence Fiber-Optic Flow Sensor for Resin Transfer AH42 Molding 6. AUTHOR(S) Bruce K. Fink, Roopesh Mathur,\* and Suresh G. Advani\* 8. PERFORMING ORGANIZATION 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) REPORT NUMBER U.S. Army Research Laboratory ATTN: AMSRL-WM-MB ARL-TR-2240 Aberdeen Proving Ground, MD 21005-5069 10.SPONSORING/MONITORING 9. SPONSORING/MONITORING AGENCY NAMES(S) AND ADDRESS(ES) AGENCY REPORT NUMBER 11. SUPPLEMENTARY NOTES \*University of Delaware, Newark, DE 19716 12b. DISTRIBUTION CODE 12a, DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution is unlimited. 13. ABSTRACT (Maximum 200 words) An evanescent wave fluorescence-based fiber-optic flow sensor is being investigated. This sensor is based on the interaction of a laser beam in a bare optical fiber with fluorescent probe molecules present in the resin flowing in the direction of the fiber. The electric field of the monochromatic light waves traveling in the fiber by total internal reflection penetrates outside the fiber and is called the evanescent wave field. A fluorescent probe molecule within the depth of penetration gets excited by this field and emits a characteristic fluorescent radiation that is coupled back into the fiber by the principle of reciprocity of optics. If the light at the end of the fiber is filtered for the fluorescent radiation and the intensity is recorded, it gives an estimate of the number of fluorescent probe molecules in contact with the fiber and, hence, the extent to which the fiber is covered with the resin. Preliminary experiments have shown that there is a linear correlation between the peak intensity and the length of fiber in contact with the fluid. A laboratory setup has been assembled at the University of Delaware (UD), using a photomultiplier-tube-based detector, and various experiments have been conducted to assess the effect of covered fiber length on the intensity of fluorescence using the evanescent mode of sensing and on the uses of distal mode sensing of fluorescence for detection of flow. 15. NUMBER OF PAGES resin transfer molding, fiber optics, flow sensors 16. PRICE CODE

OF REPORT

17. SECURITY CLASSIFICATION

UNCLASSIFIED

20. LIMITATION OF ABSTRACT

UL

18. SECURITY CLASSIFICATION

UNCLASSIFIED

OF THIS PAGE

19. SECURITY CLASSIFICATION

**UNCLASSIFIED** 

OF ABSTRACT

INTENTIONALLY LEFT BLANK.

#### USER EVALUATION SHEET/CHANGE OF ADDRESS

	USER EVALUATION SHEET	CHANGE OF ADDRESS	
This Laboratory undertake the items/questions below v	s a continuing effort to improve the quality will aid us in our efforts.	ality of the reports it published	es. Your comments/answers to
1. ARL Report Number/A	uthorARL-TR-2240 (Fink)	Date of Re	eport June 2000
2. Date Report Received _			
	a need? (Comment on purpose, related		
4. Specifically, how is the	report being used? (Information sour	ce, design data, procedure, so	ource of ideas, etc.)
	this report led to any quantitative savieved, etc? If so, please elaborate.		
	hat do you think should be changed to		
	Organization		
CURRENT	Name	E-mail Name	
ADDRESS	Street or P.O. Box No.		
	City, State, Zip Code		
7. If indicating a Change of Incorrect address below	f Address or Address Correction, plea	se provide the Current or Cor	rect address above and the Old
	Organization		
OLD	Name		
ADDRESS	Street or P.O. Box No.		

(Remove this sheet, fold as indicated, tape closed, and mail.)
(DO NOT STAPLE)

City, State, Zip Code

**DEPARTMENT OF THE ARMY** 

OFFICIAL BUSINESS

**BUSINESS REPLY MAIL** 

FIRST CLASS PERMIT NO 0001,APG,MD

POSTAGE WILL BE PAID BY ADDRESSEE

DIRECTOR
US ARMY RESEARCH LABORATORY
ATTN AMSRL WM MB
ABERDEEN PROVING GROUND MD 21005-5069

NO POSTAGE NECESSARY IF MAILED IN THE UNITED STATES